TLP/VF-TLP/HMM Test System TLP-3010C/3011C

Advanced TLP/HMM/HBM Solutions

1 Features

- Wafer and package level TLP/VF-TLP/HMM testing
- Ultra fast 50 Ω high voltage pulse output with typical 100 ps rise time
- Built-in HMM (IEC 61000-4-2) pulse up to ±8 kV
- High pulse output current up to ±30 A
- High speed 50 Ω trigger output for oscilloscopes (synchronous to high voltage pulse output)
- 6 programmable pulse rise times: 100 ps to 50 ns
- 8 programmable pulse widths: 1 ns to 100 ns
- Optional pulse width extender increases pulse width up to 1.6 μs in 68 programmable steps
- Fast measurement time, typically 0.2 s per pulse including one-point DC measurement between pulses
- Efficient software for system control and waveform data management
- The software can control automatic probers (Suss) for fast measurement of complete wafers
- High performance and high quality components

2 System Description

The universal TLP/VF-TLP/HMM test system TLP-3010C/3011C offers advanced features intended for the characterization of circuits, semiconductor devices and discretes like TVS, varistors, capacitors, in the high power time domain. It includes high current I-V characteristics in pulsed operation mode, turn-on/off transient characteristics of the device, breakdown effects, charge recovery effects (e.g. reverse recovery), Safe-Operating-Area (SOA) and ESD measurements. The test system is available in two basic configurations:

1. TLP-3010C high voltage pulse generator (Fig. 1)
2. TLP-3010C high voltage pulse generator combined with TLP-3011C pulse width extender (Fig. 2)

The TLP-3010C has 8 programmable pulse widths from 1 ns to 100 ns. The optional pulse width extender TLP-3011C (Fig. 2) is used to extend the pulse width up to 1.6 μs in 68 steps. The system has been optimized for high frequency performance, reliability and highly flexible fast software remote control.

Fig. 3 shows the measured waveform at the 50 Ω pulse output of the TLP-3010C (Fig. 4) recorded using a 12 GHz Tektronix® Oscilloscope TDS6124C at 40 GS/s sampling rate. The output pulse shows 100 ps rise time and low ringing. The measurement was performed with the pulse output directly connected to the oscilloscope input using high performance RF cables.

Figure 1: TLP-3010C system for 1 ns-100 ns pulse width

Figure 2: TLP-3011C pulse width extender 0.1-1.6 μs

Figure 3: Typical output pulse waveform (40 GS/s)
Fig. 5 shows typical 100 ns pulses with 800 V output voltage amplitude into 50 Ω load at different rise-time filter settings. The programmable rise times are useful to detect dv/dt dependent triggering of e.g. SCR-based devices or to suppress ringing caused by packaging or PCB parasitic inductances. The GPIB programmable pulse widths from 1 ns to 1.6 μs in 68 steps enable various device-under-test (DUT) investigations e.g. the Wunsch-Bell characteristic.

The DUT switch (Fig. 1(c)) automatically connects the DUT to the pulse generator or to the source meter for DC measurements.

The HPPI current sensor CS-0V5-A is used for standard TLP measurements. For very-fast TLP measurements <10 ns the software supports TDR algorithms for I/V measurements based on the incident and reflected signals.

Fig. 6 shows a photograph of the TLP-3010C/3011C test system including sampling oscilloscope, source meter for DC measurements and control PC. The optional wafer probe station is not shown.

The efficient software offers best-in-class measurement speed with up to 5 pulses/s, depending on scope and SMU data transfer speed, including one DC spot measurement after every pulse. Fig. 9 illustrates the main window of the software. It presents 4 graphic plots with transient waveforms, DC and I-V data, as well as the I-V data in tabular form. Up to five different data sets can be loaded simultaneously for a direct comparison of devices. Data plots can be copied to the Windows® clipboard and conveniently pasted in other applications. The software offers a calibration routine using zener diodes and resistors as reference. It automatically calibrates each scale step of the oscilloscope to eliminate possible offsets that might appear in the I-V curve when the scope scale is changed by the auto-ranging algorithm. As an option the software source code is available for customers who need to extend their existing measurement system.

3 Measurement Techniques

This section gives a brief overview of measurement techniques using the TLP-3010C/3011C TLP/VF-TLP/HMM test system.

3.1 Wafer Level TLP

Fig. 7 shows the main window of the software. It presents 4 graphic plots with transient waveforms, DC and I-V data, as well as the I-V data in tabular form. Up to five different data sets can be loaded simultaneously for a direct comparison of devices. Data plots can be copied to the Windows® clipboard and conveniently pasted in other applications. The software offers a calibration routine using zener diodes and resistors as reference. It automatically calibrates each scale step of the oscilloscope to eliminate possible offsets that might appear in the I-V curve when the scope scale is changed by the auto-ranging algorithm. As an option the software source code is available for customers who need to extend their existing measurement system.
Fig. 7 shows the block diagram of a standard wafer-level TLP measurement setup. To eliminate the error from non-zero contact resistance, a four point Kelvin method is preferred to measure the differential voltage directly at the device pads. We recommend using RF-probes of type Picoprobe® model-10, which are the same ones used in our vf-TLP setup. This allows the voltage to be measured with high bandwidth and enables fast switching between standard- and vf-TLP mode.

The sense probe tip has an integrated resistive divider, which enables the voltage to be measured with minimal parasitic loading (1 kΩ to 5 kΩ). Fig. 8 shows a photograph of the Picoprobe® model-10 force and sense probes, contacting a device with 200 μm pad pitch. The replaceable probe tips can be obtained with user specified pitch from GGB Industries®.

3.2 PCB and Package-Level TLP

For package and PCB-level TLP measurements, the PCB adapter shown in Fig. 1(b) is used to contact the DUT with short interconnection wires. A pulse rise time of 10 ns is recommended in order to avoid ringing due to the parasitic inductance of the wires.

3.3 Very Fast TLP

For VF-TLP measurements with pulse widths <10 ns, incident and reflected signals are recorded separately with a wide-band pick-off tee in the pulse-force line (see Fig. 11). The transient device response is calculated by combining the incident and reflected pulse signals numerically (TDR-s method). The device voltage is preferably measured directly with a second Picoprobe model-10 with integrated voltage dividing resistor. This assures high bandwidth and minimizes the voltage error due to parasitic contact resistance. It also eliminates the digital noise that is typical for voltage measurements of low-ohmic devices with the TDR-s method. In addition the software of the TLP-3010C performs precise de-embedding of cable loss (amplitude and phase) to enable accurate pulse measurements in the time-domain.

3.4 System Level ESD Test (HMM)

The TLP-3010C pulse generator also offers a Human Metal Model (HMM) pulse as an alternative test method to IEC 61000-4-2 with significant improved reproducibility of the test results. Fig. 12 shows the output pulse current into...
Figure 10: Wafer-level SOA measurement setup using the TLP-3010C/TLP-3011C test system

Figure 11: Wafer-level very-fast TLP setup (VF-TLP)

Figure 12: Measured 1 kV HMM output pulse into 2 Ω

a 2 Ω load at 1 kV. The pulse shape fulfills the IEC specifications. The maximum output level is ±8 kV according to the IEC 61000-4-2 standard with R=330 Ω and C=150 pF.

3.5 Safe Operating Area (SOA)

The Safe Operating Area (SOA) of active and passive devices can be easily measured using the TLP-3010C/3011C test system with variable pulse widths in the full range from 1 ns to 1.6 μs. Fig. 10 shows the wafer-level SOA measurement setup. This setup for SOA is very effective. The usually pulse sense probe at drain side is skipped and a pick-off tee is used instead. Measurement error due to pulse force probe contact resistance is small for drain currents <10 A.

Keithley SMU C including bias tee D for additional drain pre-bias is just optional. Normally not used. Use Picoprobe® Model 10 with probe tips with built-in 10 nF capacitor for DUT gate biasing. The bias tee E is optional to protect the SMU B. Pick-off tee and current sensor to be mounted as close as possible to the DUT. At the RF output port of bias tee E (50 Ω to ground) the dynamic gate voltage should be monitored with channel 4 of the sampling oscilloscope to ensure stable gate biasing.

3.6 Charge Recovery Time

In addition the test system TLP-3010C/3011C offers a measurement setup for charge recovery measurements like forward and reverse recovery time of diodes. In contrast to existing measurement techniques the recovery times can be measured extremely fast and efficient in the range from about 200 ps up to 1 μs. The DUT is mounted in a true 50 Ω test fixture.

Fig. 14 shows the block diagram of a 50 Ω recovery measurement setup. The DUT is operated with 50 Ω source resistance. The setup can be used for reverse as well as...
forward recovery time measurements. The DUT voltage is measured with a wideband pick-off tee. For expected recovery times <2 ns the DUT current is extracted using a VF-TLP setup. For expected recovery times >2 ns the DUT current can be measured directly with the fast-rise-time HPPI CS-0VS-A current sensor in a classical TLP setup.

To operate the DUT with a 100 Ω source resistance a 50 Ω resistor can be easily connected in series with the DUT. 50 Ω source resistance of the TLP-3010C and 50 Ω load resistance of the DUT results in total 100 Ω. In this case the DUT will be operated into a 50 Ω load or attenuator. The DUT current can be measured directly with the 50 Ω sampling oscilloscope input.

Fig. 15 shows typical reverse recovery measurement waveforms. The extraction of the reverse recovery time \( t_{rr} \) can be done as follows:

1. Set the TLP-3010C pulse parameters to 100 ps rise time and a pulse width which is approximately two to three times the expected reverse recovery time.

2. Operate diode in forward mode with a specified forward bias current \( I_F \).

3. Apply a reverse mode TLP pulse with a defined reverse voltage \( V_R = V_{TLP} - |V_F| \). The Voltage \( V_R \) is measured using the mean value between 70 % and 80 % of the TLP pulse width at the device \( V_{DUT} \).


5. Extract 25 % of the nominal peak reverse current.

6. The time where the current \( I_{DUT} \) decreases down to 25 % of the nominal peak reverse current is the reverse recovery time.

Fig. 16 shows the result which can be achieved just by three classical TLP sweeps:

\[
\begin{align*}
J_F &= 1.4 \times 10^{-6} \text{ A/\mu m}^2 \\
J_F &= 4.1 \times 10^{-6} \text{ A/\mu m}^2 \\
J_F &= 6.8 \times 10^{-6} \text{ A/\mu m}^2 
\end{align*}
\]
4 TLP-3010C/3011C Front and Rear Panel Connectors

Figure 17: TLP-3010C/3011C front panel electrical connections

Figure 18: TLP-3010C/3011C rear panel electrical connections
5 Specifications

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Symbol</th>
<th>Limit Values</th>
<th>Unit</th>
<th>Remarks</th>
</tr>
</thead>
<tbody>
<tr>
<td>Output voltage (open load)</td>
<td>$V_{\text{out, max}}$</td>
<td>-1.5</td>
<td>+1.5</td>
<td>kV into open load</td>
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<tr>
<td>Output voltage (50 Ω load)</td>
<td>$V_{\text{out,50}}$</td>
<td>-0.75</td>
<td>+0.75</td>
<td>kV into 50 Ω load</td>
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<tr>
<td>Peak pulse output power (50 Ω load)</td>
<td>$P_{\text{out,50}}$</td>
<td>11</td>
<td>kW</td>
<td>into 50 Ω load</td>
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<td>Minimum output voltage step size</td>
<td>$V_a$</td>
<td>0.1</td>
<td>V</td>
<td>into open load, GPIB progr.</td>
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<tr>
<td>Maximum TLP output current</td>
<td>$i_{\text{tp}}$</td>
<td>-30</td>
<td>+30 A</td>
<td>short circuit</td>
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<tr>
<td>Maximum TLP output current</td>
<td>$i_{\text{tp}}$</td>
<td>-15</td>
<td>+15 A</td>
<td>50 Ω load</td>
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<td>Maximum HMM first peak output current</td>
<td>$i_{\text{peak}}$</td>
<td>-30</td>
<td>+30 A</td>
<td>short circuit DUT, 50 Ω HMM</td>
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<td>Maximum HMM broad peak output current</td>
<td>$i_{\text{I2ns}}$</td>
<td>-16</td>
<td>+16 A</td>
<td>short circuit DUT, 50 Ω HMM, equivalent to ±8 kV IEC 61000-4-2 (330 Ω, 150 pF)</td>
</tr>
<tr>
<td>Output pulse rise time</td>
<td>$t_r$</td>
<td>0.1</td>
<td>50 ns</td>
<td>GPIB programmable 6 steps, out of: 0.1 / 0.3 / 0.6 / 1 / 2 / 5 / 10 / 20 / 50 ns (custom selectable)</td>
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<tr>
<td>Pulse width base unit TLP-3010C (typical)</td>
<td>$t_p$</td>
<td>1</td>
<td>100 ns</td>
<td>GPIB programmable in 8 steps: 1 / 2.5 / 5 / 10 / 25 / 50 / 75 / 100 ns</td>
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<tr>
<td>Pulse width with optional extender TLP-3011C (typ.)</td>
<td>$t_p$</td>
<td>1</td>
<td>1600 ns</td>
<td>GPIB programmable in 68 steps: 125 - 1600 ns in 25 ns steps</td>
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<td>Measurement pulse repetition time</td>
<td>$t_m$</td>
<td>200</td>
<td>500 ms</td>
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<td>AC line voltage range</td>
<td>$V_{\text{AC}}$</td>
<td>100</td>
<td>240 V</td>
<td>47-63 Hz, max. 1.8 A</td>
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<tr>
<td>Dimensions TLP-3010C (W x H x D)</td>
<td>$D_{\text{3010C}}$</td>
<td>428 (482.6) x 132.5 x 485 mm$^3$</td>
<td>428 mm body, 482.6 mm rack flange</td>
<td></td>
</tr>
<tr>
<td>Dimensions TLP-3011C (W x H x D)</td>
<td>$D_{\text{3011C}}$</td>
<td>428 (482.6) x 132.5 x 485 mm$^3$</td>
<td>428 mm body, 482.6 mm rack flange</td>
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<td>Weight TLP-3010C</td>
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<td>excluding accessories</td>
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<td>Weight TLP-3011C</td>
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<td>15.7</td>
<td>kg</td>
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<td>Software support of digital oscilloscopes</td>
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<td></td>
<td></td>
<td>All models from Keysight, LeCroy, Tektronix. New models will be added on request.</td>
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<tr>
<td>Software support of SMU source meters</td>
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<td>Keithley 24xx/26xx series SMU, Keithely 230 voltage source. Agilent B2900A. 5 SMUs can be controlled by the system: 1 leakage measurement SMU and 4 independent bias SMU.</td>
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<tr>
<td>Supported automatic probe stations</td>
<td></td>
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<td>all Suss Cascade and Signatone probe stations</td>
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<tr>
<td>Certification marks</td>
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<td></td>
<td></td>
<td>The TLP-3010C and TLP-3011C are in line with:</td>
</tr>
<tr>
<td></td>
<td></td>
<td></td>
<td></td>
<td>1. the requirements set forth in the Code of Federal Regulations CFR 47, Part 15, Sections 15.107 and 15.109 (Class A) of the Federal Communication Commission (FCC) and the Interference-Causing Equipment Standard (ICES-003) Issue 4, Sections 5.2 and 5.4 (Digital Apparatus) of Industry Canada (IC).</td>
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